

DETERMINATION OF DYNAMIC COEFFICIENT OF FRICTION FOR SOME MATERIALS FOR FEED PELLET UNDER DIFFERENT VALUES OF PRESSURE AND TEMPERATURE

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ABSTRACT

Knowledge of frictional characteristics of materials is required for equipment design. The force of friction must be overcome before these materials flow. The objective of this study is to determine the dynamic coefficient of friction " μ_d " for yellow corn grits, wheat bran, soybean meal, cotton seed meal and mixtures of some of these materials used for manufacturing pellet for cattle animals, under different values of pressure and temperature. A device was developed for determining the dynamic coefficient of friction under pressure ranging from 9 kPa up to 109 kPa and temperature ranging from 30 to 150 °C. The value of " μ_d " was determined at ten levels of pressure "P": 9, 18, 27, 42, 53, 65, 75, 88, 97 and 109 kPa, and six levels of the temperature "T": 30, 50, 75, 100, 125 and 150 °C.

The determined values of " μ_d " ranged from 0.113 to 0.397 for Yellow corn grits, from 0.122 to 0.505 for wheat bran, from 0.105 to 0.410 for cotton seed meal, from 0.105 to 0.347 for soybean meal and from 0.391 to 0.105 for mixtures of these materials.

The empirical results obtained from the carried out experiments were used to introduce a group of contour charts, using "Excel program" to predict the value of " μ_d " for the different tested material as a function of both pressure and temperature. These empirical results were also used to derive six mathematical equations to predict the value of " μ_d " as a function of both pressure and temperature. Also, one general mathematical equation was derived to predict the value of " μ_d " as a function of raw material contents (protein, ash and moisture content), material pressure and temperature.

Keywords: *Dynamic coefficient of friction, Pressure, Temperature, Yellow corn grits, Wheat bran, Soybean meal, Cotton seed meal.*

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INTRODUCTION

Fricition is defined as phenomenon existing in the contact region of two bodies moving with respect to each other. The problem of the correct description of this phenomenon is very important both from the point of view of engineering practice and the design of new machines as well as the optimisation of many technological processes. Coefficients of friction are influenced by numerous factors. Knowledge about the role of many of these factors is still incomplete, and additional experimental work is needed to determine the limits of uncertainty and to explicate the behavior of material in various conditions.

Overcoming the static force of friction is necessary to start motion. Once the motion is started, the force needed for overcoming the frictional forces to maintain motion is reduced. The friction forces existing between the surfaces of relative motion are called forces of dynamic friction (*Halling, 1975*).

Fairfield (2003) stated that the pelleting – the most intensive capital and energy consuming feed manufacturing operation – is a key driver in feed mill profitability. While pelleting of feed can provide many significant benefits, the pelleting operation is cost-effective.

Miguel and Guillermo (2002) reported that for densification of biomass, it is important to know the parameters that influence the extrusion process which are moisture content, compaction pressure, temperature and size of particles, these are the required parameters of raw materials.

Mohsenin (1970) investigated the reasons of variation in the coefficient of friction values of biological materials. The experimental results showed that sliding surface, moisture content, velocity, normal pressure, temperature, humidity and operating technique affected friction values.

Many researchers have attempted to measure the mechanical friction coefficient in a laboratory setting. *Shukla et al. (2005) and Rosentrater et al. (2005)* mentioned that the coefficient of friction is the most important rheological property. During extrusion processing, (under high compacting pressure), the bio based feed materials turn into pseudo

plastic melt and the moisture contents of ingredient mix, and the cooking temperature significantly affects the coefficient of friction and thus the extrudate properties.

Molenda et al. (2002) investigated the coefficients of friction of wheat, for grain–on–grain, and on galvanized corrugated steel sheet using a modified direct shear apparatus. They conducted the tests under a normal pressure of 20.7 kPa using soft red winter wheat at a moisture content of 11.2% (w.b.) and an uncompressed bulk density of 740 kg/m³. Test results of grain–on–grain coefficients of friction was 0.47, while for grain on steel sheet was 0.56.

Faruk Taser et al. (2005) found that the measured values of coefficient of dynamic friction against hard-wood sheet, galvanized steel, mild steel, chipboard and rubber surfaces were 0.29, 0.30, 0.33, 0.33, and 0.41 respectively for Hungarian vetch seed

Rusinek and Molenda (2007) studied the coefficient of friction of rapeseed according to Eurocode (kinetic) in direct shear test and (static) in model silo. Samples of rapeseed in a range of moisture content from 6 to 15% (w.b.) were used and the tests were performed for galvanized steel, stainless steel and concrete. Coefficient of friction for both steel types approached stable value for all levels of moisture content in a range from 0.11 to 0.18. For concrete, it was found in a range from 0.25 to 0.43. The coefficient of static friction found in model silo decreased with an increase in vertical pressure from 0.3 to 0.2 for first loading, while in subsequent loading cycles, it decreased from 0.2 to 0.1.

Grift et al. (2006) determined the dynamic mechanical friction coefficient of individual urea fertiliser particles in real time. A method based on theoretical analysis was proposed. The analysis showed that the friction coefficients can be measured using a single radial velocity measurement per particle. The friction coefficients found for urea fertilizer showed a near-Gaussian distribution with a mean of 0.36.

Ghadge et al (2008) found that the static coefficient of friction varied for Chick Pea on three different surfaces from 0.30 on galvanized steel sheet, 0.43 on Plywood to 0.45 on glass.

Ahmadi et al. (2008) found that the static coefficient of friction varied for apricot fruits on four different surfaces from 0.62 on galvanized steel sheet, 0.51 on wood, 0.55 on fiberglass sheet to 0.49 on glass

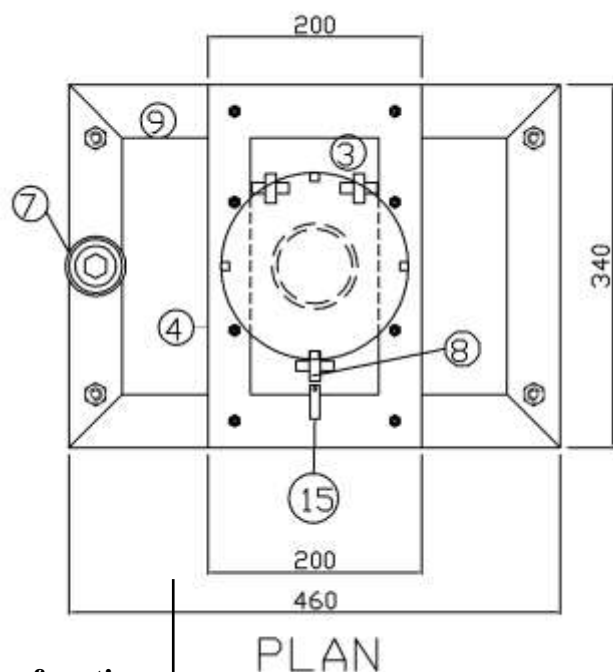
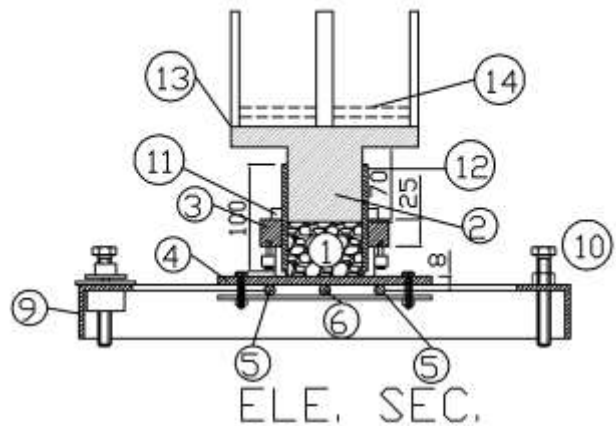
The objective of this study was concentrated on the determination of the dynamic coefficient of friction for six feed materials used for manufacturing pellet for the cattle animals (yellow corn grits, wheat bran, soybean meal, cotton seed meal and two mixtures from these materials) on steel 50 under different values of compacting pressure and temperature.

MATERIALS AND METHODS

This research work was conducted in Agric. Eng. Dept. Faculty of Agriculture - Cairo University during the year 2008. The method followed was developed and guided to some extent from the method described by (*Mohsenin 1970*). A device was designed and fabricated then it was used for the determination of the dynamic coefficient of friction for six materials

The device Fig. (1) mainly consists of: two open sides cylinder threaded from its outer side to adjust it, up and down, by a nut resting on a carriage surface. The carriage has a horizontal plate surface 275×120×20 mm and fixed to three roll bearing wheels, one in the front and 2 in the back to support the carriage. Under this design, the cylinder down open side could be adjusted to be very close to a third part which is a metallic surface made of steel 50 (200 mm wide, 350 mm length and 10 mm thickness), but without touching it. This steel 50 surface was mounted on a horizontal steel base of 50 mm height, to allow fixing the heating element and thermostat very close to the down face of steel 50 surface to control its temperature as required.

The two open sides cylinder is partially filled with the tested sample of the feed materials. The feed material is compressed by a cylindrical rod (a piston), 40 mm in diameter and 70 mm in depth. A 600 Watt heater was fixed very close to the down face of the sliding surface and was provided by a thermostat to adjust temperature.



Direction of motion ↓

- | | | |
|------------------------------|---------------------|-----------------------|
| 1-Sample | 2- Piston | Dims. in mm |
| 4- Sliding surface | 5- Heater | 3- Carriage |
| 7- Thermostat | 8- Rolling wheels | 6- Temperature sensor |
| 10- Adjustable screw | 11- Adjustable nut | 9- Base |
| 13- Cage for loading weights | 14- Loading weights | 12- Cylinder |
| | | 15- Bar pull |

Fig. (1): The designed device for measuring the dynamic friction force.

The upper surface of the piston is fixed to a steel cage in which load weights are put to resemble the compacting pressing forces existing on the feed material inside any extruder producing the feed material pellet.

The carriage is connected through a pivoting point to a 250 N load measuring transducer. The transducers cell is attached to a digital force gauge (Japanese made) to measure the needed pulling force to move the carriage to oppose the dynamic friction force between the sample and steel surface to maintain the motion. Fig. (1) shows this designed device. This locally designed and fabricated device was used to measure the dynamic friction force between feed material and the friction surface (steel 50).

All metallic surfaces were cleaned by compressed air before each test to remove any contamination from any previous tests. Sliding steel surface was horizontally adjusted by applying a bubble level fixed on the base to insure eliminating the effect of any force resulting from slopes. (The result when sample is pulled, the pulling force will represent only the frictional force.)

Treatments:

1. Types of food material

Six types of feed materials used for feeding cattle were tested: Yellow corn grits, wheat bran, Soybean meal, Cotton seed meal , and two recommended mixtures by the cattle breeders which are mixture (1) (50 % corn, 25 % wheat bran, 5 % Soybean meal, 20 % Cotton seed meal) and mixture (2) (40 % corn, 35 % wheat bran, 10 % Soybean meal, 15 % Cotton seed meal).

The chemical components of the tested feed materials were determined according to *NRC (2001)*. The chemical components are shown in table (1). It was found that the percentage of protein, fat content, total carbohydrates, crude fiber, ash and moisture content for the tested materials ranged between (8.40 to 38.01 %), (3.33 to 4.13 %), (32.68 to 72.36 %), (2.28 to 10.68 %), (1.14 to 5.48 %) and (10.21 to 12.50 %), respectively.

Table (1): Chemical components of the tested materials.

Feed materials	<i>Pr</i> , %	<i>F</i> , %	<i>Car</i> , %	<i>Fib</i> , %	<i>Ash</i> , %	<i>MC</i> , %
Yellow corn	8.40	3.33	72.36	2.28	1.14	12.50
<i>Wheat bran</i>	13.44	3.45	57.30	8.84	5.39	11.58
<i>Cotton seed meal</i>	36.81	4.13	32.68	10.68	5.48	10.21
<i>Soybean meal</i>	38.01	3.99	36.06	5.23	5.32	11.39
<i>Mixture (1)</i>	16.82	3.55	58.85	5.75	3.28	11.76
<i>Mixture (2)</i>	17.39	3.56	57.51	6.13	3.70	11.72

Pr = Protein content,
Fib = Crude fiber,

F = Fat content,
Ash = Ash,

Car = Carbohydrates,
MC = Moisture content

Particle Size Distribution:

A 100 g sample of each material was placed in a stack of sieves arranged downward from the largest to the smallest opening. The sieve series selection was based on seven sizes of particles in the sample. Sieve analysis was repeated three times for each ground samples. The particle size was determined according to ANSI/ASAE standard S319.3JUL97 (ASAE, 2002).

The mass percentages distribution of the particle size of Yellow corn grits, wheat bran, Soybean meal, Cotton seed meal are shown in table (2).

Table (2): Size distribution of feed material.

Feed materials	Percentage of Particle size, (%)						
	Particle size (mm)						
	2 - 3	2 - 1	1 - 0.5	0.5 - 0.25	0.25-0.125	0.125 - 0.053	< 0.053
Yellow corn	54.21	24.02	10.79	6.11	3.39	1.19	0.28
<i>Wheat bran</i>	13.69	29.66	41.52	14.21	0.52	0.31	0.10
<i>Cotton meal</i>	58.13	23.21	11.48	4.95	1.87	0.36	-
<i>Soybean meal</i>	36.88	26.52	6.39	8.87	14.12	6.46	0.76

Moisture content "MC_{d.b}"

Moisture content was determined as dry base for materials (table 1).

2. Pressure "P"

The tested values of pressure were: 9, 18, 27, 42, 53, 65, 75, 88, 97 and 109 kPa, which resulting from normal load imposed on the sample over the area of the cylinder.

3. Temperature "T"

Six levels of the temperature were tested: 30, 50, 75, 100, 125 and 150 °C. The temperature of the sliding surface was measured by a digital infrared thermometer.

The dynamic coefficient of friction was determined by applying equation (1):

$$\mu d = F_r / N_l \dots\dots\dots(1)$$

Where:

μd = dynamic coefficient of friction;

F_r = Friction force, kg_f ;

N_l = Normal load pressing the food material to the surface of contact, kg_f.

Three replicates were conducted for each of the tested treatments. The friction force was measured using digital force gauge (accuracy ± 10 gm). Microsoft Excel and SPSS software programs regression method were applied for data analysis.

RESULTS AND DISCUSSIONS

1. Effect of pressure "P" and temperature "T" on the dynamic coefficient of friction " μd " between the tested materials and steel 50:

The values of the dynamic coefficient of friction " μd " for Yellow corn grits, wheat bran, Soybean meal, Cotton seed meal, mixture (1) and mixture (2) are shown in table (3-a), table (3-b) and Fig. (2). These results show that " μd " decreased by increasing the pressure "P" and by increasing the temperature "T" for any tested material.

The reason why wheat bran had the highest dynamic coefficient of friction at 30 °C, may be due to that its moderate size particles > 0.5 and ≤ 2.0 mm, (table 2), which could be more rough and stable under low pressing force had the highest percentage. Although both corn grits and the cotton seed meal had higher percentages of the rough particles 2 – 3 mm, but they were not stable, and large protein of its rough extrusions were easily broken, and became smoother. Under higher compressing force, all the materials particles became smoother and had low dynamic coefficient of friction.

Also, table (1) shows that the "fat" in all the tested materials had a percentage of almost 3 to 4 percent. Under higher temperature, the viscosity of the "fat" decreases and it acts as a lubricant agent. That is the reason why under higher values of temperature the value of the dynamic coefficient of friction dramatically decreases for all the tested materials and under any compressing force. The reason for decreasing in dynamic coefficient of friction, due to the increase in pressure may be due to that compressed material could form a smooth compacted surface layer sliding easier on the surface of contact. Similar observations were offered by *Thompson and Ross (1983)*, since they applied normal pressure in a range from 7 to 172 kPa. These authors observed in tests performed for wheat against steel a decrease in the coefficient of friction with an increase in normal pressure, a similar tendency was observed by *Rusinek and Molenda (2007)* when testing the coefficient of friction for rapeseed with steel in a pressure range from 20 to 60 kPa.

The obtained results for the effect of pressure and temperature on dynamic coefficient of friction, Table (3-a) and (3-b), were used to have both a graphical set of charts and a set of mathematical equations to predict the value of the dynamic coefficient of friction for different tested feed material against "steel 50", as function of both pressure and temperature.

Table (3- a): The effect of pressure and temperature on the dynamic coefficient of friction.

Material	T, °C	Pressure, kPa									
		9	18	27	42	53	65	75	88	97	109
Corn	30	0.397	0.315	0.280	0.265	0.259	0.257	0.253	0.244	0.243	0.243
	50	0.379	0.268	0.249	0.209	0.189	0.177	0.178	0.173	0.169	0.169
	75	0.347	0.240	0.208	0.172	0.151	0.142	0.139	0.134	0.136	0.131
	100	0.315	0.240	0.193	0.165	0.144	0.137	0.131	0.124	0.125	0.120
	125	0.315	0.246	0.182	0.162	0.141	0.133	0.130	0.124	0.119	0.113
	150	0.303	0.233	0.178	0.158	0.135	0.128	0.120	0.114	0.113	0.113
Wheat bran	30	0.505	0.489	0.432	0.374	0.330	0.301	0.290	0.262	0.249	0.236
	50	0.385	0.290	0.260	0.192	0.178	0.159	0.154	0.157	0.154	0.153
	75	0.347	0.240	0.217	0.165	0.151	0.151	0.147	0.141	0.142	0.137
	100	0.328	0.240	0.215	0.165	0.146	0.142	0.139	0.137	0.139	0.129
	125	0.315	0.278	0.215	0.159	0.141	0.138	0.135	0.131	0.132	0.128
	150	0.303	0.249	0.193	0.158	0.135	0.134	0.131	0.124	0.125	0.122
Cotton seed meal	30	0.410	0.309	0.262	0.225	0.216	0.217	0.214	0.199	0.199	0.188
	50	0.315	0.246	0.217	0.174	0.157	0.146	0.139	0.131	0.132	0.129
	75	0.284	0.230	0.195	0.166	0.151	0.133	0.131	0.124	0.128	0.122
	100	0.259	0.215	0.193	0.159	0.144	0.124	0.124	0.118	0.119	0.116
	125	0.240	0.196	0.184	0.158	0.141	0.120	0.120	0.111	0.116	0.113
	150	0.208	0.170	0.152	0.144	0.135	0.115	0.116	0.110	0.113	0.105

Table (3-b): The effect of pressure and temperature on the dynamic coefficient of friction.

Material	T, °C	Pressure, kPa									
		9	18	27	42	53	65	75	88	97	109
Soy meal	30	0.347	0.268	0.249	0.231	0.225	0.217	0.209	0.209	0.205	0.191
	50	0.284	0.237	0.219	0.185	0.165	0.149	0.146	0.141	0.135	0.129
	75	0.265	0.205	0.193	0.166	0.151	0.142	0.133	0.124	0.128	0.122
	100	0.252	0.183	0.172	0.159	0.144	0.137	0.127	0.121	0.120	0.105
	125	0.221	0.170	0.163	0.158	0.151	0.136	0.127	0.118	0.113	0.105
	150	0.189	0.151	0.148	0.137	0.135	0.135	0.128	0.118	0.113	0.105
Mixture (1)	30	0.391	0.268	0.217	0.203	0.192	0.186	0.185	0.173	0.172	0.169
	50	0.315	0.237	0.206	0.168	0.157	0.142	0.139	0.131	0.132	0.129
	75	0.284	0.215	0.197	0.166	0.151	0.142	0.133	0.126	0.128	0.122
	100	0.252	0.205	0.195	0.159	0.144	0.133	0.124	0.121	0.116	0.105
	125	0.221	0.189	0.184	0.179	0.146	0.134	0.122	0.118	0.115	0.113
	150	0.189	0.183	0.178	0.158	0.145	0.135	0.120	0.118	0.113	0.105
Mixture (2)	30	0.284	0.221	0.195	0.185	0.179	0.167	0.162	0.160	0.160	0.169
	50	0.189	0.174	0.156	0.151	0.145	0.133	0.131	0.131	0.131	0.129
	75	0.177	0.151	0.148	0.144	0.141	0.128	0.127	0.124	0.120	0.122
	100	0.151	0.142	0.141	0.126	0.124	0.120	0.117	0.114	0.119	0.105
	125	0.139	0.132	0.130	0.117	0.114	0.111	0.112	0.112	0.113	0.105
	150	0.126	0.120	0.119	0.113	0.108	0.105	0.116	0.118	0.107	0.105

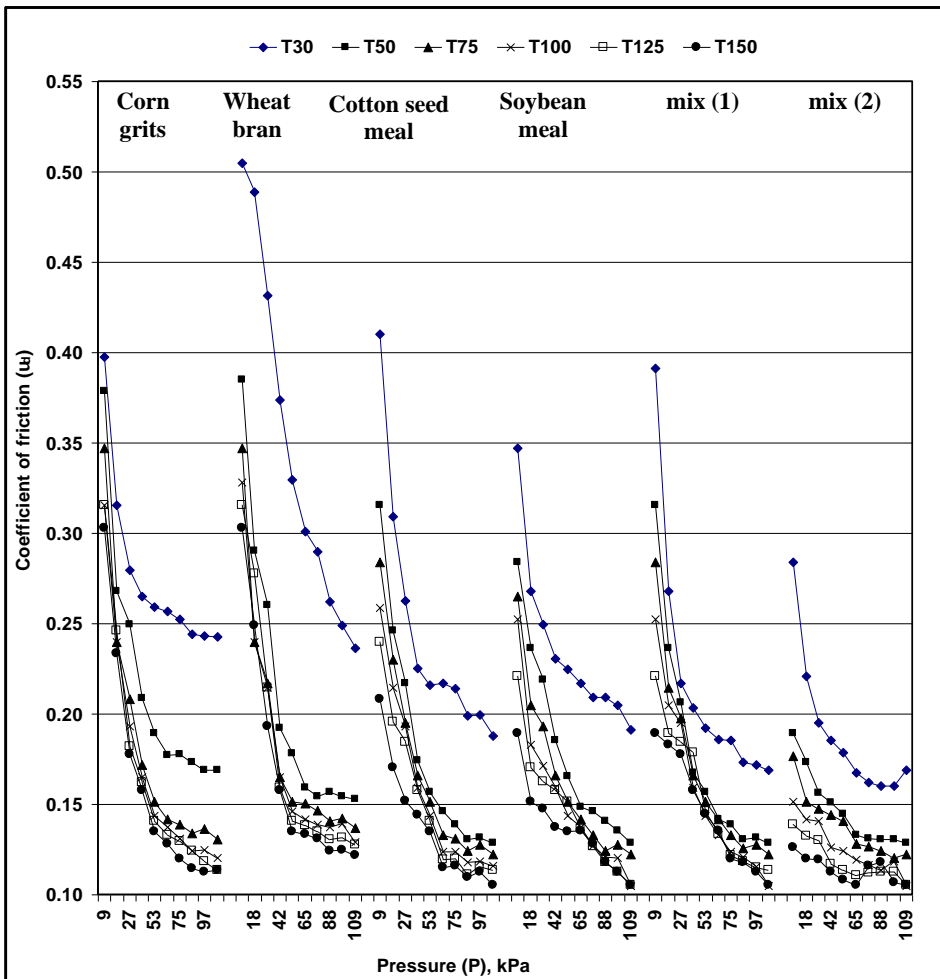


Fig. (2): Effect of pressure and temperature on the dynamic coefficient of friction between steel 50 and different feed materials.

Dynamic coefficient of friction " μ_d " contour charts

For corn grits, a relation was derived between both temperature and pressure in one side and the dynamic coefficient of friction " μ_d " on the other side, by transferring the data of Table (3) into a spread sheet (Excel program) to draw a surface contour charts relating the values of the dynamic coefficient of friction " μ_d " by both the (pressure x-axis) and the (temperature y-axis), Fig. (3).

Fig. (3) shows the contour lines limiting each selected or needed range values of the dynamic coefficient of friction " μ_d ". Fig. (3) could be applied to find out the value of " μ_d " corresponding to both the value of pressure and the value of temperature.

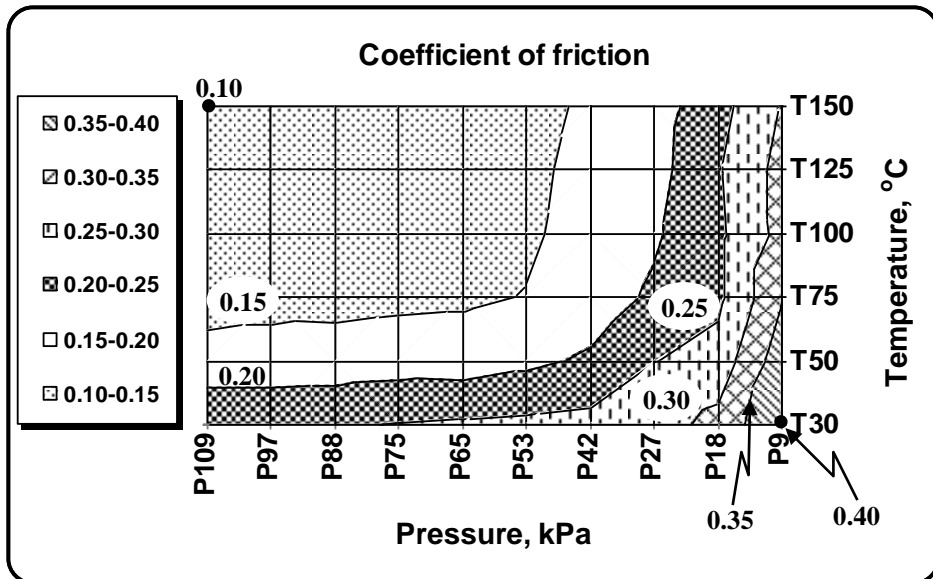


Fig. (3): Effect of pressure "P" and temperature "T" on the dynamic coefficient of friction " μ_d " between yellow corn grits and steel 50.

Also, applying the same above technique, contour charts could be drawn for the dynamic coefficient of friction between steel 50 and other feed materials, Fig. (4) shows the chart for wheat bran, Fig. (5) shows the chart for cotton seed meal, Fig. (6) shows the chart for soybean meal, Fig. (7) shows the chart for mixture (1) and Fig. (8) shows the chart for mixture (2).

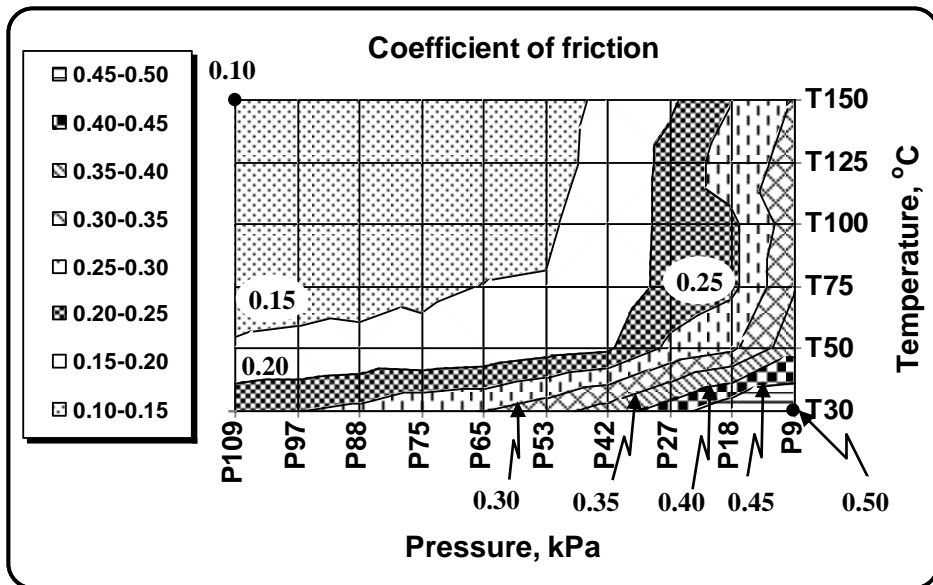


Fig. (4): Effect of pressure "P" and temperature "T" on the dynamic coefficient of friction " μ_d " between wheat bran and steel 50.

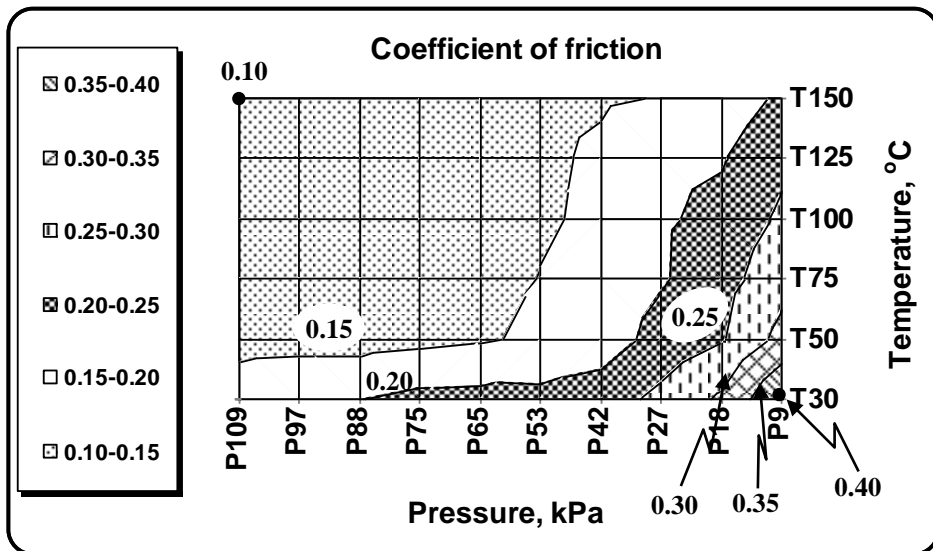


Fig. (5): Effect of pressure "P" and temperature "T" on the dynamic coefficient of friction " μ_d " between cotton seed meal and steel 50.

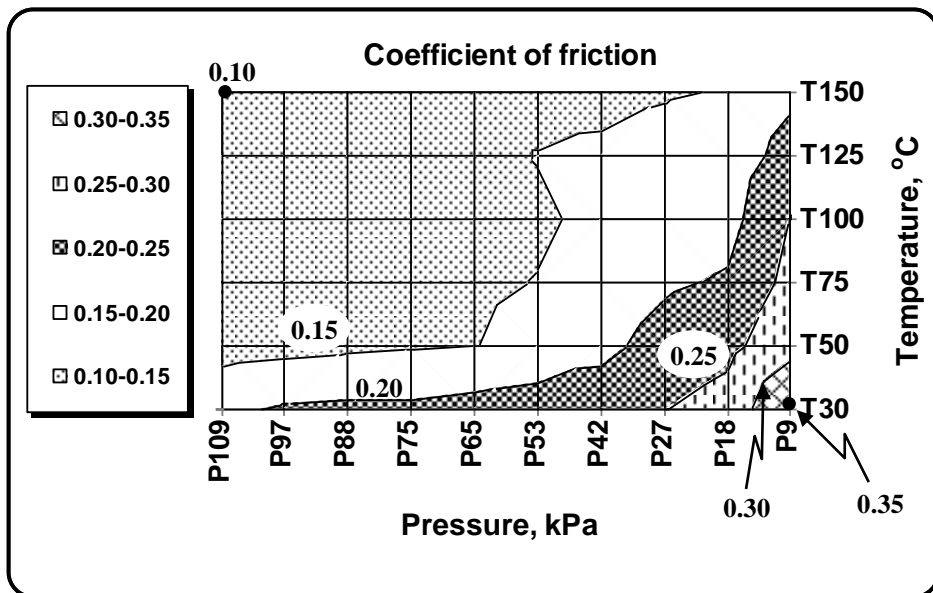


Fig. (6): Effect of pressure "P" and temperature "T" on the dynamic coefficient of friction " μ_d " between soybean seed meal and steel 50.

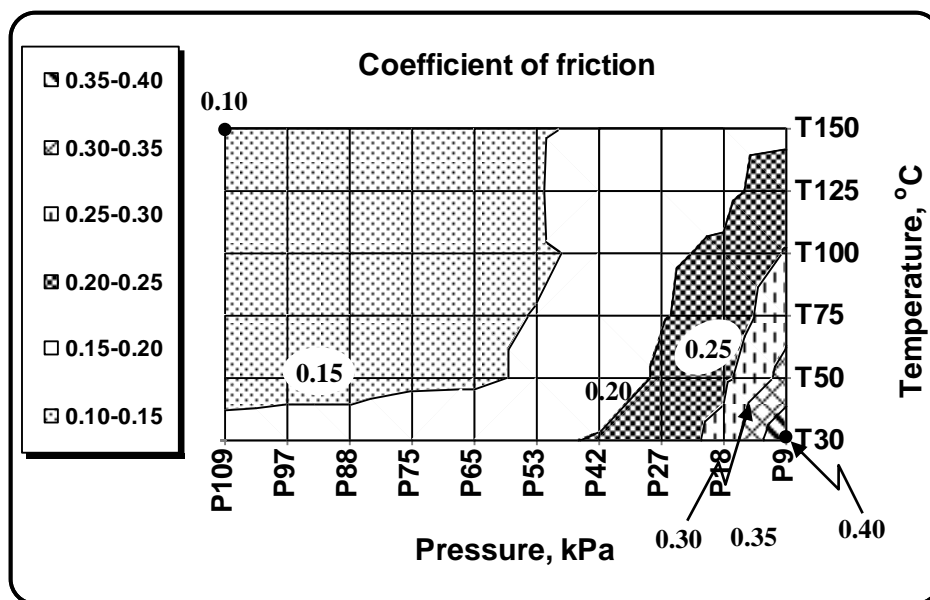


Fig. (7): Effect of pressure "P" and temperature "T" on the dynamic coefficient of friction " μ_d " between mixture (1) and steel 50.

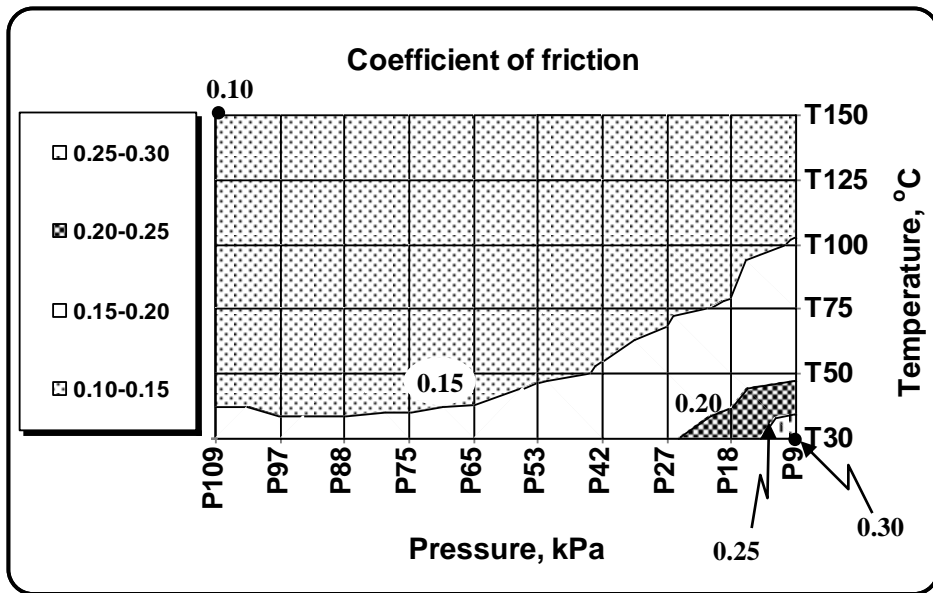


Fig. (8): Effect of pressure "P" and temperature "T" on the dynamic coefficient of friction " μ_d " between mixture (2) and steel 50.

2. The mathematical expression of the effect of pressure "P" temperature "T" and feed chemical components on dynamic coefficient of friction between the tested materials and steel 50:

The above mentioned graphical technique for finding out the value of the dynamic coefficient of friction " μ_d ", could be replaced by another mathematical technique applying multiple regression approach to find out the value of dynamic coefficient of friction " μ_d " as a function of both pressure, temperature and feed chemical component.

2.1 Mathematical expression for the effects of "P" and "T" on the value of " μ_d " by applying the multiple regression approach:

Multiple regression approach was used to derive a regression equation (2), expressing the effects of the pressure "P" and temperature "T" on the dynamic coefficient of friction " μ_d "

$$\mu d = a \times P + b \times T + k \dots\dots\dots(2)$$

Where

- μd = dynamic coefficient of friction.
- P = Pressure pressing the feed material to the surface of contact, kPa; ($9 \leq P \leq 109$).
- T = Temperature, °C; ($30 \leq T \leq 150$).
- a, b, k = Empirical constants.

The values of the empirical constants (a, b and k) and the coefficient of determination of equation (3) are shown in table (4).

Table (4): The empirical constants and the coefficient of determination of equation 2 for the six tested materials.

Material	Empirical constant			R ²
	A	b	k	
Yellow corn	$- 1.542 \times 10^{-3}$	$- 8.554 \times 10^{-4}$	0.360	0.723
Wheat bran	$- 1.870 \times 10^{-3}$	$- 1.139 \times 10^{-3}$	0.420	0.670
Soybean meal	$- 1.074 \times 10^{-3}$	$- 7.000 \times 10^{-4}$	0.293	0.786
Cotton seed meal	$- 1.340 \times 10^{-3}$	$- 7.285 \times 10^{-4}$	0.315	0.754
Mixture (1)	$- 1.284 \times 10^{-3}$	$- 5.063 \times 10^{-4}$	0.288	0.754
Mixture (2)	$- 4.631 \times 10^{-4}$	$- 5.449 \times 10^{-4}$	0.214	0.729

2.2 Mathematical expression for the effects of P, T and the feed chemical components (protein, fat, carbohydrates, fiber, ash and moisture content) on the values of "μd" by applying the multiple regression approach:

The obtained results of table (1) for the chemical components of the tested materials were used as factors affecting the values of the dynamic coefficient of friction. So, multiple regression approach (by using SPSS software) was used to derive a regression equation expressing the effects of the pressure "P", the temperature "T", protein, fat, carbohydrates, fiber, ash and moisture content on the value of the dynamic coefficient of friction "μd". The results of this analysis were reviewed to exclude the variables which had minor effects. The excluded variables are fat content, carbohydrates and fiber.

Equation (3) expresses this mathematical relation:

$$\mu d = a \times P + b \times T + c \times Pr + d \times Ash + e \times MC + k \dots \dots \dots (3)$$

where

- μd = dynamic coefficient of friction
- P = Pressure pressing the feed material to the surface of contact, kPa; ($7 \leq P \leq 52$)
- T = Temperature, °C; ($30 \leq T \leq 150$)
- Pr = Protein content; % ; ($0.92 \leq Pr \leq 11.6$)
- Ash = Ash; % ; ($0.53 \leq Ash \leq 24.42$)
- MC = Moisture content; %; ($10.21 \leq MC \leq 12.5$)

a, b, c, d, e & k = Empirical constants

$$a = -1.262 \times 10^{-3}, \quad b = -7.456 \times 10^{-4}, \quad c = -1.183 \times 10^{-3},$$

$$d = 6.478 \times 10^{-3}, \quad e = 1.923 \times 10^{-3}, \quad k = 0.292, \quad R^2 = 0.601$$

Thus, equation (4) can be used to predict the dynamic coefficient of friction of any feed materials resembling those tested materials or any other materials, under different values of pressure and temperature with in the domain of the tested conditions.

CONCLUSION

From this investigation the following conclusions could can be made:

1. The dynamic coefficient of friction " μd " of the tested materials decreased by increasing both the pressure imposed on the tested materials and its temperature.
2. A maximum value of " μd ", 0.505, was found for wheat bran at 9 kPa and 30 °C.
3. A minimum value of " μd ", 0.105, was found for cotton seed meal soy meal and mixture at P 109 kPa and "T" from 100 to 150 °C.
4. The effect of pressure and temperature on " μd " was highly significant.
5. Graphical charts were introduced, applying Excel program to predict the values of " μd " for different tested materials and steel 50.
6. Mathematical equations applying the multiple regression technique were derived for each material (six materials) for expressing " μd " as a function of T in °C and P in kPa imposed on it.
7. The general derived regression equation (eq. 3) could be used with enough confidence in predicting the dynamic coefficient of friction

" μ d" for feed materials resembling the tested material or any other material, with the domain of the tested values which could be produced the extruders under high pressure and temperature values.

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الملخص العربي

تقدير معامل الاحتكاك الديناميكي لبعض مواد العلف الداخلة في تصنيع المصبغات تحت قيم مختلفة من الضغط ودرجة الحرارة

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يتم تصنيع بعض مواد العلف على هيئة مصبغات باستخدام البائق الحراري, الذي يعتمد في أدائه على زيادة درجة الحرارة والضغط نتيجة لاحتكاك المادة الغذائية الخام بمعدن الوحدة الفعالة للبائق الحراري, وأيضاً نتيجة للطاقة المستهلكة في التشكل البلاستيكي للمادة والطاقة المستهلكة في تحول البروتين من صورته العادية الي الطورة النسيجية.

لذلك فان هذه الدراسة تهدف الي تقدير معامل الإحتكاك الديناميكي تحت قيم مختلفة من الضغوط ودرجات الحرارة بين "الصلب ٥٠" وبين ستة مواد وهي: جريش الذرة الصفراء , الردة الناتجة من القمح, كسب بذرة القطن, كسب فول الصويا, ومخلوطين بنسبة مختلفة من المواد السابقة المستخدمة والموصى بها في تغذية الحيوانات الكبيرة.

وللوصول لهدف الدراسة, فقد تم تطوير جهاز لتقدير مقاومة الحركة الإنزلاقية للمواد المختبرة تحت تأثير قيم مختلفة من الضغوط ودرجات الحرارة نتيجة لتأثير معامل الإحتكاك الديناميكي. وقد تمت الدراسة عند عشرة مستويات للضغط وهي ٩, ١٨, ٢٧, ٤٢, ٥٣, ٦٥, ٧٥, ٨٨, ٩٧, ١٠٩ كيلوبسكال وستة مستويات لدرجة الحرارة, وهي ٣٠, ٥٠, ٧٥, ١٠٠, ١٢٥, ١٥٠ درجة مئوية لستة مواد مختلفة في التركيب البنائي لها.

و قد بينت الدراسة ما يلي:

١. يقل معامل الإحتكاك الديناميكي بزيادة الضغط و درجة الحرارة للمواد.
٢. أقصى قيمة لمعامل الإحتكاك الديناميكي كانت ٠,٥٠٥ للردة عند ضغط ٩ كيلوبسكال, و درجة حرارة ٣٠ درجة مئوية.
٣. أقل قيمة لمعامل الإحتكاك الديناميكي كانت ٠,١٠٥ لكسب القطن وفول الصويا ومخلوط مواد العلف (١), (٢) عند ضغط ١٠٩ كيلوبسكال, و درجة حرارة تتراوح من ١٠٠ الى ١٥٠ درجة مئوية.
٤. كان لكل من الضغط ودرجة الحرارة تأثير عالى المعنوية علي معامل الإحتكاك الديناميكي .
٥. تم التوصل الى خرائط كنتورية باستخدام برنامج الاكسيل وذلك للتنبؤ بقيم معامل الاحتكاك الديناميكي لمواد العلف التي تم اختبارها مع الصلب ٥٠.
٦. تم التوصل الي ستة معادلات رياضية بطريقة الإنحدار الخطي لكل مادة من المواد المختبرة الستة تعبر عن معامل الإحتكاك الديناميكي كدالة لكل من درجة الحرارة بالدرجات المئوية و الضغط الواقع على المواد المختبرة بوحدات الكيلوبسكال.
٧. كذلك تم التوصل الي معادلة عامة بطريقة الإنحدار الخطي للتنبؤ بمعامل الإحتكاك الديناميكي تحت الضغوط المقدره بالكيلوبسكال كالتى تحدث في الباتق الحرارى على المواد المصنعة - ودرجة الحرارة مقدره بالدرجات المئوية - ونسب المكونات الكيميائية للمواد المصنعة وهي نسبة البروتين ونسبة الرماد والمحتوى الرطوبى - وذلك لأي مادة لها مواصفات فى حدود مواصفات المواد التي تمت الدرسة عليها.