

## PERFORMANCE ASSESSMENT OF CENTER PIVOT IRRIGATION SYSTEM UNDER ARID AREAS CONDITION

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### ABSTRACT

*This study was planned to evaluate the effects of operating pressure ( $P$ ), spacing between sprinklers ( $S$ ) and height of sprinkler above the ground surface ( $H$ ) on the uniformity parameters [(coefficient of uniformity ( $CU$ ), distribution uniformity ( $DU_{Iq}$ ) and coefficient of variation ( $CV$ )] under center pivot system. The quantitative variables were ( $P_{20, 40}$  and  $60$ ), ( $S_{200, 250}$  and  $300$ ) and ( $H_{150, 175}$  and  $200$ ).*

*The obtained values of  $CU$  and  $DU$  were higher under the highest  $P$ , closer  $S$  and higher  $H$ . In contrast,  $CV$  was lower under the highest  $P$ , closer  $S$  and higher  $H$ . Both  $CU$  and  $DU_{Iq}$  were increased with increasing the  $P$  and  $S$ ,  $P$  and  $H$  and decreasing  $S$  with an increase  $H$ . While the  $CV$  decreased with increasing the  $P$  and  $S$ ,  $P$  and  $H$ . Also, decreasing  $S$  and increase  $H$ .*

*The highest  $CU$  values were recorded when the center pivot was operated under ( $P_{60, S_{200}}$  and  $H_{200}$ ) and ( $P_{40, S_{200}}$  and  $H_{200}$ ) without significant differences between them. Also, the highest  $DU$  and the lowest  $CV$  were recorded when the center pivot was operated under ( $P_{40, S_{200}}$  and  $H_{200}$ ). So, it is recommended to operate the center pivot at ( $P_{40, S_{200}}$  and  $H_{200}$ ) to save the pumping costs in studied area and similar conditions.*

**Keywords:** Center pivot, Uniformity parameters, Operating pressure, Spacing between sprinklers and Height of sprinklers.

### INTRODUCTION

**W**ith response to the increase in water scarcity created by rising demands in several sectors and slowing down of new water source development, irrigated agriculture, the largest user of water in most semi-arid countries is under significant pressure to reduce water consumption.

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Technical solutions to the growing phenomenon of water scarcity abound, and governments throughout the world have undertaken commitments to reduce water use in agriculture by improving the efficiency of water use in that sector (Brennan, 2008). Application efficiency can be increased by adopting pressurized irrigation system like sprinkler irrigation (Rana *et al.*, 2006).

Center pivot irrigation systems are often preferred by farmers due to its robustness and automation possibilities (Hanson and Orloff, 1996 and Dechmiet *et al.*, 2003); low labor requirements and ability to irrigate large fields (Kincaid, 2005); easier operation and have the capacity to attain highly uniform and efficient irrigation results in water saving and farm profitability (Tarjuelo *et al.*, 1999).

The uniformity coefficients are often determined from measurements with water collection cans located above the crop on bare soil (Mateo *et al.*, 1997). Two methods have been developed to quantify uniformity, CU and the distribution uniformity (DU). Coefficient of uniformity (CU) is one of the first criteria defined to express uniformity. This coefficient is derived from catch-can data assuming that the catch-cans represent the same area. It is a measure of the absolute difference from the mean divided by the mean. Distribution uniformity (DU) is usually defined as a ratio of the smallest accumulated depths in the distribution to the average depths of the whole distribution. The largest depths could also be used to express DU, but since the low values in irrigation are more critical, the smallest values are used (Burt *et al.*, 1997). Distribution uniformity emphasizes the areas which receive the least of irrigation water by focusing on the low quarter ( $DU_{lq}$ ). They suggested the  $DU_{lq}$  is expressed as a decimal. Thus, both CU and  $DU_{lq}$  coefficients give complementary information. Uniformity is increased when the two coefficients (CU and  $DU_{lq}$ ) are closer (Ortiz *et al.*, 2010).

In addition, the coefficient of variation (CV) in application volume can be computed as the standard deviation of all catch can measurements divided by the average catch can volume for a test. Both  $DU_{lq}$  and CU have been related to the CV analytically (Warrick, 1983) and verified

experimentally on center pivot irrigation machines (Heermann *et al.*, 1992 and Dukes, 2006).

Distribution uniformity with center pivot systems mainly depends on the sprinkler unit, the type or size of sprinklers and spacing along the lateral, the height above the ground or canopy, plot topography, and the speed of the machine in order to avoid run-off (Allen *et al.*, 2000).

Tarjuelo *et al.* (1999) reported that there was a negative correlation between DU and P. Moazed *et al.* (2010) found that the CU value was increased by increasing P. They added that relation was not linear and with lower P, the slope was steeper. Keller (1983) reported that, in a given sprinkler as the P lowers, the dispersion is intensified and water drops hit the ground greater, but this will decrease the water distribution, also, the relatively excessive sprinkled water in the predefined dispersion range. Pressure enhancement will decrease excessive sprinkled water leading to an improved water distribution uniformity coefficient. Therefore he suggested that the lower P occurs when sprinkler spacing is lower.

Water distribution uniformity increases when H is increased (Hills and Barragan 1998 and Tarjuelo *et al.*, 1999 Alazba *et al.*, 2004). Increased height gives a larger wetted diameter for the same nozzle type and size, and consequently the overlap percentage is increased and the water application uniformity along the lateral is improved (Allen *et al.*, 2000). Increasing H usually produces better irrigation uniformity for a specific wind speed and direction, but it also increases evaporation and drift losses (Faciet *et al.*, 2001). Installing the sprinkler at a lower height reduces the wetted area and increases the application rate (Keller and Bliesner, 1990 and Faciet *et al.*, 2001).

Moazed *et al.* (2010) studied the effect of S on CU under solid set system. Also, (Clark *et al.*, 2003) studied the effect of S on CU under center pivot system. They reported that the elongated spacing between sprinkler decreasing CU value.

The objective of this study was to quantify the operating effect of some factors influencing the water distribution uniformity under center pivot irrigation system. In addition, a set of recommendations will be given for

management of center pivot system for Sebha region and other environmentally similar regions.

### **MATERIALS AND METHODS**

Field evaluations were conducted on center pivot irrigation system to quantify the effect of some operating factors influencing the water distribution uniformity under Sebha region, south of Libya- conditions. The evaluations were carried out in October 2010 on bare soil to avoid the plant interference of applied water. The experiment was done during 09:00 and 12:00 in an attempt to coincide with low temperature and evaporation conditions as well as lower wind speed.

The center pivot system is a 250 m length, five spans (where span is defined as the pipeline and support truss between two support towers), each span is 50 m length. The total irrigated area was 19.6 ha. Fixed spray plate sprinklers (FSPS) were used along the spans with the overhang of the center pivot.

The catch can test is a commonly used to assess the uniformity of sprinkler systems. Standards have been developed for determining the uniformity of water distribution of center pivot (ASAE, 2001). All collectors used in the test to measure the depth of water applied was identical and shaped such that water does not splash in or out. The lip of the collector was symmetrical and without depressions.

Catch cans with a 10 cm opening diameter and a 15 cm height were used. The catch can tests were conducted on the outer of the center-pivot irrigation systems (spans three, four and five), which represents 60% of the total irrigated area. So, catch cans began 100 m from the center pivot point and the spacing between cans was 1 m. There were 90 catch cans along a line. This line was far away from the pipeline to allow the system achieve working conditions before arriving at the test site. The catch can reading process was carried out as quickly as possible with the aim of reducing evaporation losses in collectors. The water depth collected was calculated by dividing the volume caught by the open area of the catch can.

The FSPS were placed at 200cm above the ground ( $H_{200}$ ) in the third span, at 175cm ( $H_{175}$ ) in the fourth span and 150 cm ( $H_{150}$ ) in the fifth span (Fig.1). The spaced between sprinklers (S) were 200, 250 and 300cm ( $S_{200}$ ,  $S_{250}$  and  $S_{300}$ ) apart in each span. The operating pressures (P) at the fixed center pivot point were 20, 40 and 60 bar ( $P_{20}$ ,  $P_{40}$  and  $P_{60}$ ).

In order to avoid the overlapping effect between treatments under each span, two borders conducted between three spacing treatments. Five m between each two spacing treatments were considered and 2.5 m at the two ends of each span. So, each spacing treatment has a 10 m (Fig.1). All treatments were conducted at 50 % rotation speed.

The  $CU$ ,  $DU_{lq}$  and  $CV$  values for each span were calculated for evaluating center pivot irrigation system.

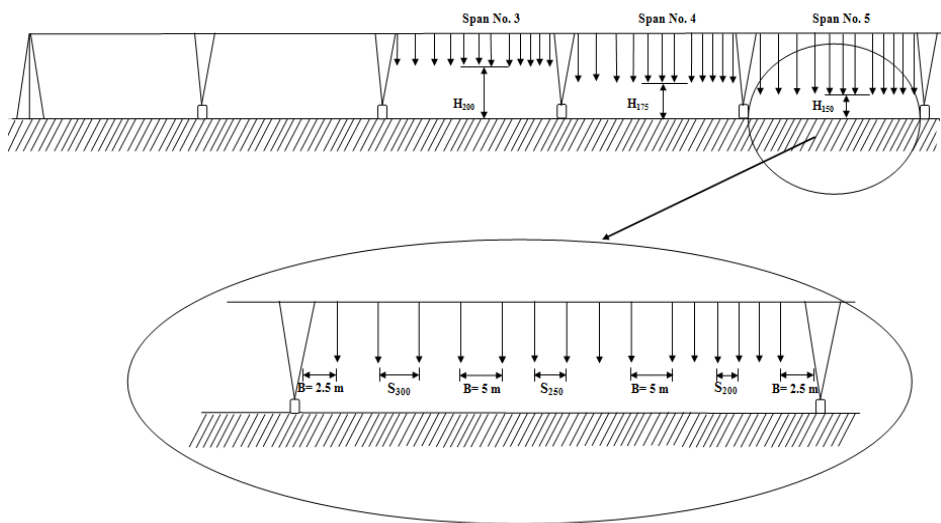


Fig. (1): Diagram of the positioning of sprinklers on the span.

### Evaluation of Uniformity:

Several quantitative analyses procedures of water uniformity were used. These uniformities were calculated by the following equations:

#### 1- Coefficient of uniformity (CU):

The center pivot coefficient of uniformity was calculated using the modified formula of Heermann and Hein (1968) given by (ASAE, 2001):

$$CU = \left[ 1 - \frac{\sum_{i=1}^n S_s \left| D_s - \frac{\sum_{i=1}^n D_s S_s}{\sum_{i=1}^n S_s} \right|}{\sum_{i=1}^n D_s S_s} \right] \times 100$$

Where:

- $D_s$  water depth (mm) collected by a catch can to a distance  $S$  from the center pivot.
- $s$  a subscript that denotes the position to a distance  $S$ .
- $n$  number of the catch can.

## 2- Distribution uniformity ( $DU_{lq}$ ):

The low quarter irrigation distribution uniformity ( $DU_{lq}$ ) was calculated using the following equation (Merriam and Keller 1978):

$$DU_{lq} = \frac{ADC_{25}}{ADC} \times 100$$

Where:

- $ADC_{25}$  lowest quarter of the average water depth of a group of catch-can measurements.
- $ADC$  total average water depth of a group of catch-can measurements.

## 2- Coefficient of variation (CV):

The coefficient of variation (CV) is the quotient between the standard deviation of the applied water depths at the different points of the field ( $\sigma$ ) and the average of water depth collected:

$$CV = \frac{\sigma}{D_s}$$

Where:

- $\sigma$  the standard deviation of the applied water.
- $D_s$  the average of water depth collected.

This experiment was designed as a split-split-plot design with three replicates. The operating pressure ( $P_{20,40}$  and  $60$ ) was arranged in main plots, the sprinkler spacing ( $S_{200, 250}$  and  $300$ ) were allocated in the sub-plots, while sprinkler height ( $H_{150, 175}$  and  $200$ ) were allocated in the sub-sub-plots. The obtained data were statistically analyzed using SPSS software program (2008). Differences between means were compared by LSD at 5% level (Gomez and Gomez. 1984).

## RESULTS AND DISCUSSION

### 1- Effect of quantitative variables on CU and $DU_{iq}$

Data illustrated in Tables (1 and 2) focused the significant influence of P, S, H and their interactions on CU and  $DU_{iq}$  parameters. However, CU was significantly with increasing the P. The same trend was recorded for  $DU_{iq}$  but the increment was insignificant.

The highest P ( $P_{60}$ ) gained acceptable CU and  $DU_{iq}$  values comparing to  $P_{20}$  and  $P_{40}$  (Tables, 1 and 2). Over all testing conditions, under  $P_{60}$ ,  $P_{40}$  and  $P_{20}$ , the average CU values were 83.19, 81.00 and 76.20%, while those of  $DU_{iq}$  were 0.785, 0.759 and 0.703, respectively.

Table (1): The effects of operating pressure, spacing between sprinklers and height of sprinkler above the ground surface on coefficient of uniformity (CU) values.

Pressure (bar)	Spacing (cm)			Sprinkler height (cm)			
				150	175	200	
20	200			<b>71.26</b>	<b>80.05</b>	<b>90.72</b>	
	250			<b>67.17</b>	<b>75.18</b>	<b>84.76</b>	
	300			<b>63.37</b>	<b>71.44</b>	<b>82.12</b>	
	Average			<b>67.27</b>	<b>75.55</b>	<b>85.86</b>	
40	200			<b>75.02</b>	<b>87.00</b>	<b>93.93</b>	
	250			<b>71.83</b>	<b>82.39</b>	<b>89.66</b>	
	300			<b>65.30</b>	<b>79.69</b>	<b>84.15</b>	
	Average			<b>70.72</b>	<b>83.03</b>	<b>89.25</b>	
60	200			<b>76.32</b>	<b>89.12</b>	<b>94.67</b>	
	250			<b>74.94</b>	<b>86.04</b>	<b>90.09</b>	
	300			<b>69.50</b>	<b>81.50</b>	<b>86.54</b>	
	Average			<b>73.59</b>	<b>85.55</b>	<b>90.43</b>	
Average of spacing	200			<b>74.20</b>	<b>85.39</b>	<b>93.11</b>	
	250			<b>71.31</b>	<b>81.20</b>	<b>88.17</b>	
	300			<b>66.06</b>	<b>77.54</b>	<b>84.27</b>	
	Average			<b>70.52</b>	<b>81.38</b>	<b>88.52</b>	
LSD 0.05 for:	<b>P</b>	<b>S</b>	<b>H</b>	<b>P×S</b>	<b>P×H</b>	<b>S×H</b>	<b>P×S×H</b>
	<b>1.13</b>	<b>1.13</b>	<b>1.13</b>	<b>1.43</b>	<b>1.43</b>	<b>1.43</b>	<b>2.17</b>

Regarding sprinkler spacing (S) effect on CU and  $DU_{iq}$  values decreased with increasing SS. CU values decreased by 5.02 and 10.89 % when SS was increased to  $S_{250}$  and  $S_{300}$ , the corresponding values for  $DU_{iq}$  were 8.36 and 14.34%, respectively. This result is full agreements with (Clark

*et al.*, 2003 and Moazed *et al.*, 2010). They reported that, CU values tended to decrease with increasing sprinkler spacing.

Tables (1 and 2) show that CU and  $DU_{iq}$  were increased with increasing H. CU values increased by 15.39 and 25.48 % when H was increased to  $H_{175}$  and  $H_{200}$ , respectively. However, the highest and lowest values of CU were recorded at sprinkler height  $H_{200}$  and  $H_{150}$ , respectively. This result occurred because some soil points received larger amount of water, whereas water distribution at other points was very scarce. This trend was also shown by Allen *et al.* (2000), Faciet *et al.* (2001) and Alazba *et al.* (2004). As shown in Table (2) the average values of  $DU_{iq}$  overall H were 0.647, 0.757 and 0.843 for  $H_{150}$ ,  $H_{175}$  and  $H_{200}$ , respectively. This means that  $DU_{iq}$  was increased by 16.99 and 30.21% as sprinkler height increased to  $H_{175}$  and  $H_{200}$ , respectively.

As showed in Tables (1 and 2) the different dual interactions between the quantitative variables were significant.

Table (2): The effects of operating pressure, spacing between sprinklers and height of sprinkler above ground surface on distribution uniformity ( $DU_{iq}$ ) values.

Pressure (Bar)	Spacing (cm)			Height (cm)			Average
				150	175	200	
20	200			<b>0.661</b>	<b>0.760</b>	<b>0.867</b>	<b>0.763</b>
	250			<b>0.627</b>	<b>0.647</b>	<b>0.773</b>	<b>0.682</b>
	300			<b>0.577</b>	<b>0.640</b>	<b>0.777</b>	<b>0.665</b>
	Average			<b>0.622</b>	<b>0.682</b>	<b>0.806</b>	<b>0.703</b>
40	200			<b>0.680</b>	<b>0.813</b>	<b>0.933</b>	<b>0.809</b>
	250			<b>0.630</b>	<b>0.793</b>	<b>0.843</b>	<b>0.755</b>
	300			<b>0.617</b>	<b>0.720</b>	<b>0.803</b>	<b>0.713</b>
	Average			<b>0.642</b>	<b>0.775</b>	<b>0.860</b>	<b>0.759</b>
60	200			<b>0.717</b>	<b>0.880</b>	<b>0.920</b>	<b>0.839</b>
	250			<b>0.680</b>	<b>0.820</b>	<b>0.860</b>	<b>0.787</b>
	300			<b>0.637</b>	<b>0.743</b>	<b>0.810</b>	<b>0.730</b>
	Average			<b>0.678</b>	<b>0.814</b>	<b>0.863</b>	<b>0.785</b>
Average of spacing	200			<b>0.686</b>	<b>0.818</b>	<b>0.907</b>	<b>0.803</b>
	250			<b>0.646</b>	<b>0.753</b>	<b>0.825</b>	<b>0.741</b>
	300			<b>0.610</b>	<b>0.701</b>	<b>0.797</b>	<b>0.703</b>
	Average			<b>0.647</b>	<b>0.757</b>	<b>0.843</b>	
LSD 0.05 for:	<b>P</b>	<b>S</b>	<b>H</b>	<b>P×S</b>	<b>P×H</b>	<b>S×H</b>	<b>P×S×H</b>
	<b>NS</b>	<b>0.117</b>	<b>0.117</b>	<b>0.171</b>	<b>0.171</b>	<b>0.171</b>	<b>0.242</b>



Both CU and  $DU_{lq}$  were increased with increasing both the P and S. The lowest P ( $P_{20}$ ), caused reduction in throw radius. These reductions in radius of throw would result in sprinkler overlap changing this will reduce the water distribution uniformity. Under  $S_{200}$  and different P ( $P_{20}$ ,  $P_{40}$  and  $P_{60}$ ), the uniformity parameter values of CU were 80.67, 85.32 and 86.70%, (Table, 1). The corresponding values for  $DU_{lq}$  were 0.763, 0.809 and 0.839 (Table, 2), respectively. At the highest spacing ( $S_{300}$ ) the uniformity parameter values were 72.31, 76.38 and 79.18% for CU and 0.665, 0.713 and 0.730 for  $DU_{lq}$ , respectively in the same order. The highest CU values 85.32 and 86.70% were recorded at  $P_{40}$  and  $P_{60}$  at  $S_{200}$ . But the difference between CU resulted from  $P_{40}$  and  $P_{60}$  (85.32 and 86.70%) was not significant. Thus, to save the pumping costs, it's recommended to operate the center pivot at  $P_{40}$ . It's clear from Table (1), that in the case of the closer spacing ( $S_{200}$ ), to obtain the acceptable CU, operate the center pivot at lower P ( $P_{20}$ ) to gain CU = 80%. This result is in an agreement with Keller, (1983). He suggested that the lower P occurs when S is lower.

To obtain the highest CU under combinations of P and S parameters, center pivot irrigation system has to operate at pressure  $P_{40}$  and  $S_{200}$  (the difference between CU resulted from  $P_{40}$  and  $P_{60}$  (85.32 and 86.70%) was not significant.).

Data in Tables (1 and 2) illustrate the data of grouped P and H where the CU and  $DU_{lq}$  increased by increasing P and H. The lowest CU and  $DU_{lq}$  values (67.27% and 0.622) were recorded under low P and H ( $P_{20}$  and  $H_{150}$ ), respectively. The highest CU and  $DU_{lq}$  values (90.43% and 0.863) were recorded under high P and H ( $P_{60}$  and  $H_{300}$ ), respectively.

Under  $H_{200}$  and both  $P_{40}$  and  $P_{60}$  the highest CU (89.25 & 90.43%) and  $DU_{lq}$  (0.860 & 0.863) were recorded. The difference between CU and  $DU_{lq}$  values resulted from  $P_{40}$  and  $P_{60}$  was insignificant. Also, to save the pumping costs, it's recommended to operate the center pivot at  $P_{40}$ . To obtain the highest CU and  $DU_{lq}$  under grouped P and H conditions, and at the same time save the pumping cost, the center pivot must operate at pressure  $P_{40}$  and  $H_{200}$ .

From Tables (1 and 2) the CU and  $DU_{lq}$  values were increased by increasing H and decreasing S. The lowest CU and  $DU_{lq}$  values (66.06 %

and 0.610, respectively) were recorded under the lowest H ( $H_{150}$ ) and the widest S ( $S_{300}$ ). The highest CU and  $DU_{1q}$  values (93.11% and 0.907) were recorded under the highest H ( $H_{200}$ ) and closer S ( $S_{200}$ ). To obtain the height CU and  $DU_{1q}$  (93.11 % and 0.907, respectively) under grouped H and S conditions sprinklers must be install at  $S_{200}$  and  $H_{200}$ . Fig (2) show that, under  $S_{200}$ , when the H was increased from  $H_{150}$  to  $H_{175}$  and  $H_{200}$  the CU values increased by 15.08 & 25.49%, while those of  $DU_{1q}$  were 19.24 & 32.22%, respectively.

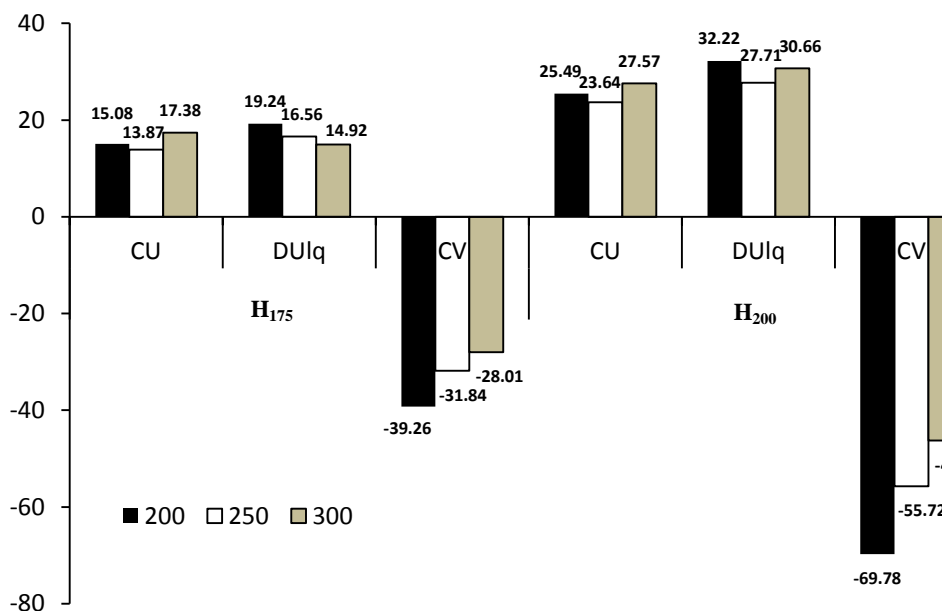


Fig. (2): The percentage of uniformity parameters under  $H_{175}$  and  $H_{200}$  compared to  $H_{150}$  one.

As shown in Tables (1 and 2) the trio-interactions between the quantitative variables were significant. The highest CU values (94.67 and 93.93 %) were recorded when the center pivot operated under ( $P_{60}$ ,  $H_{200}$  and  $S_{200}$ ) and ( $P_{40}$ ,  $S_{200}$  and  $H_{200}$ ), respectively without significant differences between them. While, the lowest CU value (63.37%) was recorded when operate the center pivot under  $P_{20}$ ,  $H_{150}$  and  $S_{300}$ . So,

to save the pumping costs, it's recommended to operate the center pivot at ( $P_{40}, S_{200}$  and  $H_{200}$ ) (Table, 1).

The highest  $DU_{1q}$  value (0.933) was recorded when the center pivot operated under  $P_{40}, S_{200}$  and  $H_{200}$ , while the lowest one (0.577) was recorded at  $P_{20}, S_{300}$  and  $H_{150}$  (Table, 2).

From Tables (1 and 2), it's clear also that, when the center pivot was operated under both  $H_{200}$  and  $S_{200}$  at different P treatments ( $P_{20}, P_{40}$  and  $P_{60}$ ) gained the highest CU ( $CU > 90\%$ ) and  $DU_{1q}$  ( $DU_{1q} > 0.867$ ).

## 2- Effect of quantitative variables on CV:

Data illustrated in Table (3) focused on the significant influence of P, S, H and their interactions on CV. The CV value was significantly decreased with increasing each P and H, but increased with increased with increasing spacing between sprinklers.

Table (3): The effects of operating pressure, spacing between sprinklers and height of sprinkler above the ground surface on coefficient of variance (CV) values.

Pressure (bar)	Spacing (cm)			Height (cm)			Average
				150	175	200	
20	200			<b>35.39</b>	<b>23.69</b>	<b>12.97</b>	<b>24.02</b>
	250			<b>38.36</b>	<b>28.82</b>	<b>19.30</b>	<b>28.83</b>
	300			<b>40.58</b>	<b>33.53</b>	<b>23.84</b>	<b>32.65</b>
	Average			<b>38.11</b>	<b>28.68</b>	<b>18.70</b>	<b>28.50</b>
40	200			<b>27.92</b>	<b>16.16</b>	<b>6.98</b>	<b>17.02</b>
	250			<b>33.23</b>	<b>20.94</b>	<b>13.06</b>	<b>22.41</b>
	300			<b>37.91</b>	<b>25.00</b>	<b>19.39</b>	<b>27.43</b>
	Average			<b>33.02</b>	<b>20.70</b>	<b>13.14</b>	<b>22.29</b>
60	200			<b>26.24</b>	<b>14.54</b>	<b>7.12</b>	<b>15.97</b>
	250			<b>28.00</b>	<b>18.12</b>	<b>11.74</b>	<b>19.29</b>
	300			<b>33.44</b>	<b>22.07</b>	<b>16.94</b>	<b>24.15</b>
	Average			<b>29.23</b>	<b>18.24</b>	<b>11.93</b>	<b>19.80</b>
Average of spacing	200			<b>29.85</b>	<b>18.13</b>	<b>9.02</b>	<b>19.00</b>
	250			<b>33.20</b>	<b>22.63</b>	<b>14.70</b>	<b>23.51</b>
	300			<b>37.31</b>	<b>26.86</b>	<b>20.05</b>	<b>28.08</b>
	Average			<b>33.45</b>	<b>22.54</b>	<b>14.59</b>	<b>23.53</b>
LSD 0.05 for:	<b>P</b>	<b>S</b>	<b>H</b>	<b>P×S</b>	<b>P×H</b>	<b>S×H</b>	<b>P×S×H</b>
	1.12	1.12	1.12	1.41	1.41	1.41	2.15

CV value at the lowest height  $P_{20}$  was higher than those at  $P_{40}$  and  $P_{60}$  by 27.86 and 43.94%, respectively. Also, CV at the lowest sprinkler height ( $H_{150}$ ) was higher than those at  $H_{175}$  and  $H_{200}$  by 48.40 and 129.27 %, respectively. CV at the lowest sprinkler spacing ( $S_{200}$ ) was lower than those at  $S_{250}$  and  $S_{300}$  by 23.74 and 47.79%, respectively.

As shown in Table (3) the dual interactions between the quantitative variables were significant.

The CV decreased with increasing both P and S. Under  $S_{200}$  and different P ( $P_{20}$ ,  $P_{40}$  and  $P_{60}$ ) the uniformity parameter values were 24.02, 17.02 and 15.97 %, respectively. The corresponding values under  $S_{300}$  were 32.65, 27.43 and 24.15%, respectively in the same order.

Data grouped according to P and H (Table 3), the CV was decreased by increasing P and H. The lowest CV value (11.93%) was recorded under the highest P and H treatment ( $P_{60}$  and  $H_{200}$ ). While the highest CV value (38.11%) was recorded under the lowest P and H treatment ( $P_{20}$  and  $H_{150}$ ). Under  $H_{200}$  and both  $P_{40}$  and  $P_{60}$  was recorded the lowest CV (13.14 and 11.93, respectively). The difference between CV resulted from  $P_{40}$  and  $P_{60}$  was insignificant. Therefore, to obtain the lowest CV under grouped according to P and H conditions the center pivot must operate at pressure of  $P_{40}$  and height of  $H_{200}$ .

The interaction between S and H was significant and declare that the lowest CV value (9.02%) was recorded under the highest H ( $H_{200}$ ) and closer S ( $S_{200}$ ). While the highest CV value (37.31%) was recorded under the lowest H ( $H_{150}$ ) and the widest S ( $S_{300}$ ). To obtain the lowest CV sprinklers must be installed at  $S_{200}$  and  $H_{200}$ .

From Fig (1), under  $S_{200}$ , when the H increased from  $H_{150}$  to  $H_{175}$  and  $H_{200}$  the CV declined to -39.26% and -69.78%. The same trend was recorded under  $S_{250}$  and  $S_{300}$ .

The tri- interaction between the quantitative variables was significant. According to the interaction between the overall testing conditions the lowest CV (6.98 %) was recorded when the center was operated under  $P_{40}$ ,

H<sub>200</sub> and S<sub>200</sub> conditions. While, the highest CV (40.58%) was recorded when operate the center pivot under P<sub>20</sub>, H<sub>150</sub> and S<sub>300</sub> conditions (Table 3).

It is clear that, when operate the center pivot under both H<sub>200</sub> and S<sub>200</sub> and different P (P<sub>20</sub>, P<sub>40</sub> and P<sub>60</sub>) gained the lowest CV (CV < 12%).

### 3- Correlation coefficient:

The correlation coefficient between the uniformity parameters and the considered quantitative variables were arranged in (Table,4). The correlation coefficients between the uniformity parameters and the quantitative variables were very strong.

There were negative correlations between both the CU & DU<sub>lq</sub> and S, but it was positive with each of P and H. An opposite trend was recorded with CV. So, its correlations with both P and H were negative, while it was positive with S.

Table (4): Correlation coefficient between the uniformity parameters and the quantitative variables.

Quantitative variables	Uniformity parameters		
	CU	DU <sub>lq</sub>	CV
P	0.978	0.979	-0.971
S	-0.994	-0.991	1.000
H	0.993	0.997	-0.996

As shown in Fig. (3), the CU was consistently higher than DU<sub>lq</sub> and both are inversely related to CV. This result is on line with Keller and Bliesner (2000). They reported that, according to the mathematical relationship between CU and DU<sub>lq</sub>, CU will always be larger (when both are decimals or a percentage) since positive and negative deviations from the mean application volume are used in the calculation of CU. whereas, only negative deviations are used in the calculation of DU<sub>lq</sub>. Both DU<sub>lq</sub> and CU are linearly related to CV (Fig.3), similar results were reported

by Tarjuelo *et al.*, (1999). Warrick (1983) showed similar relationships in an analytical analysis of CU,  $DU_{lq}$ , and CV.

As shown in Fig. (3), the obtained relation between CU and  $DU_{lq}$  against CV were:

$$CU = 101.82 - 0.92 CV, R^2 = 0.99$$

$$DU_{lq} = 99.21 - 1.03CV, R^2 = 0.96$$

The relationships from the present study were close to relationships found by Heermann *et al.* (1992) and Dukes (2006) despite there were differences and variation in the testing conditions.

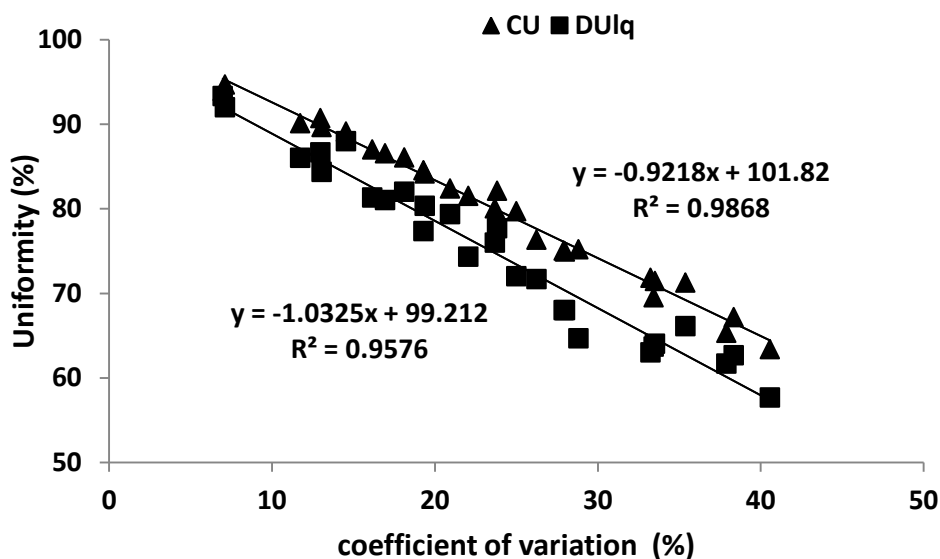


Fig. (3): Relationships between  $DU_{lq}$  and CU with (CV).

### CONCLUSIONS

From the obtained results, it is recommended to apply the highest uniformity parameters and good management of center pivot irrigation under Sebha region and other similar regions. To optimize the system performance, center-pivot should be operated under 40 bar

pressure ( $P_{40}$ ), 200 cm between sprinklers ( $S_{200}$ ) and 200 cm height of sprinklers above the ground ( $H_{200}$ ).

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الملخص العربي

## تقييم أداء نظام الري بالرش المحوري تحت ظروف المناطق الجافة

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تهدف هذه الدراسة إلى تقييم تأثير ضغط التشغيل (P)، المسافة بين الرشاشات (S) وارتفاع الرشاشات عن سطح الأرض (H) على معامل الانتظامية (CU) وابتظامية التوزيع ( $DU_{Iq}$ ) ومعامل الاختلاف (CV) تحت نظام الري بالرش المحوري. وكانت المعاملات كما يلي: ثلاثة ضغوط تشغيل ( $P_{20}$ ،  $P_{40}$  و  $P_{60}$ ) بار، ثلاثة مسافات بين الرشاشات ( $S_{200}$ ،  $S_{250}$  و  $S_{300}$ ) سم وثلاثة ارتفاعات للرشاشات عن سطح الأرض ( $H_{150}$ ،  $H_{175}$  و  $H_{200}$ ) سم. وقد أظهرت النتائج أن أعلى قيم CU و  $DU_{Iq}$  كانتا تحت ضغط التشغيل العالي (٦٠ بار) والمسافة الضيقة بين الرشاشات (٢٠٠ سم) والمسافة الأعلى للرشاشات عن سطح الأرض (٢٠٠ سم). بينما كان على النقيض من ذلك بالنسبة لمعامل الإختلاف حيث كانت قيمته الدنيا عند قيم المتغيرات سابقة الذكر. وقد لوحظ أن CU و  $DU_{Iq}$  تزيد بزيادة ضغط التشغيل (OP) وارتفاع الرشاشات عن سطح الأرض (HS) وأيضاً بتقليل المسافة بين الرشاشات (SS). بينما تقل بزيادة OP وHS وبتقليل SS. كما أظهرت النتائج أنه لا يوجد فرق معنوي في قيم معامل التوزيع عند تشغيل النظام على ( $OP_{60}$  و  $SS_{200}$  و  $HS_{200}$ ) و ( $OP_{40}$  و  $SS_{200}$  و  $HS_{200}$ ) في حين سجلت أعلى قيم  $DU_{Iq}$  وأقل قيمة CV عند تشغيل النظام على ( $OP_{40}$  و  $HS_{200}$ ) و ( $SS_{200}$  و  $HS_{200}$ ). وعلية توصى الدراسة بتشغيل نظام الري بالرش المحوري تحت ظروف منطقة الدراسة والمناطق المماثلة مناخياً عند ( $OP_{40}$  و  $SS_{200}$  و  $HS_{200}$ ) وذلك لتقليل تكاليف التشغيل.

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